


E 24 Reihe

1.0 | 1.1 | 1.2 | 1.3 | 1.5 | 1.6 | 1.8 | 2.0 | 2.2 | 2.4 | 2.6 | 2.9 | 3.2 |
3.5 | 3.8 | 4.2 | 4.6 | 5.1 | 5.6 | 6.2 | 6.8 | 7.5 | 8.3 | 9.1

| | | | | | | | |
|--------|--------|--------|-----------|-------------|-----------|------------|------------|
| Giga | Mega | Kilo | Milli | Mikro μ | Nano | Piko | Femto |
| 10^9 | 10^6 | 10^3 | 10^{-3} | 10^{-6} | 10^{-9} | 10^{-12} | 10^{-15} |

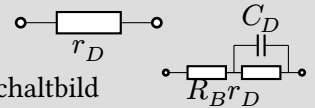
Knotenregel, $\sum I = 0$ Maschenregel $\sum U = 0$
 Parallelwiderstände $R_1 \parallel R_2 = \frac{1}{\frac{1}{R_1} + \frac{1}{R_2}} = \frac{R_1 \cdot R_2}{R_1 + R_2}$
 Spannungsteiler $U_2 = U \cdot \frac{R_2}{R_1 + R_2}$
 Stromteiler $I_1 = I \cdot \frac{R_2}{R_1 + R_2}$
 3 dB-Grenzfrequenz $f_{3dB} = \frac{1}{2\pi \cdot C \cdot R}$

Übertragungsfunktion normiert: $\frac{1}{1+j\omega K}$ bzw. $\frac{j\omega K}{1+j\omega K}$
 $\omega_{3dB} = \frac{1}{K} \Rightarrow f_{3dB} = \frac{1}{2\pi K} \quad Z_L = j\omega L, Z_C = \frac{1}{j\omega C}$
 $|H(\omega)| = |a + bj| = \sqrt{a^2 + b^2}$

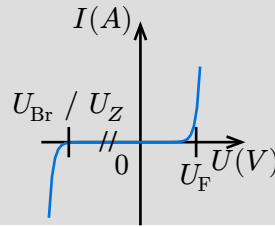
Diode 

mit $U_T = \frac{k_B \cdot T}{e} \approx 26\text{mV}$
 Diodenstrom $I_D = I_s \cdot \left(e^{\frac{U_D}{U_T}} - 1 \right)$
 Diodenspannung $U_D = U_T \cdot \ln\left(\frac{I_D}{I_s}\right)$
 Kleinsignal $r_D = \frac{U_T}{I_D}$

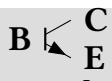
Kleinsignalersatzschaltbild



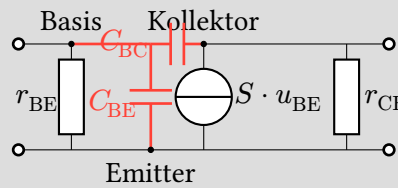
Erweitertes Kleinsignalersatzschaltbild



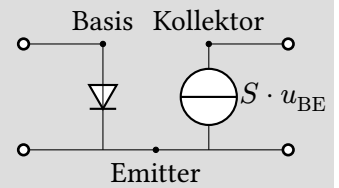
U_F Flussspannung
 U_{Br} / U_Z Durchbruchspannung / Zenerspannung

Bipolartransistor 

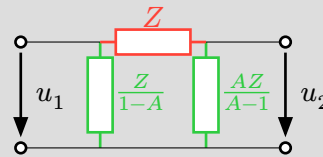
Steilheit $S = \frac{I_{C,A}}{U_{BE}}$
 Kleinsignal-Eingangs-Widerstand $r_{BE} = \frac{\beta}{S}$
 Stromverstärkung $\beta = \frac{I_C}{I_B}$
 Ausgangswiderstand $r_{CE} = \frac{|U_A| + U_{CE}}{I_C}$



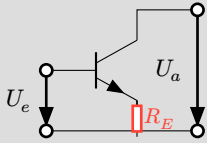
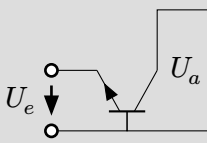
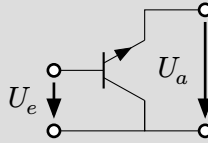
vollständiges Kleinsignalersatzschaltbild



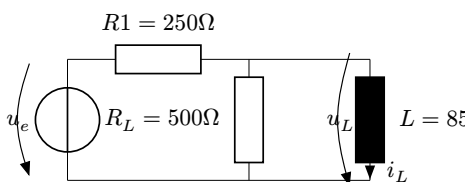
Großsignalersatzschaltbild



Miller-Theorem: $A = \frac{u_2}{u_1}$
 verbundene Impedanz Z wird zu zwei getrennte Impedanzen

| Ermitterschaltung | Basisschaltung | Kollektorschaltung |
|---|---|---|
|  |  |  |
| $A = -SR_C$ $r_e = r_{BE}$ $r_a = r_{CE} \parallel R_C$ Stromgegenkopplung $A = -\frac{R_C}{R_E}$ $r_e = r_{BE}$ $r_a = r_{CE} \parallel R_C$ | $A = SR_C$ $r_e = \frac{1}{S}$ $r_a = r_{CE} \parallel R_C$ | $A = 1$ $r_e = r_{BE} + \beta R_E$ $r_a = \frac{1}{S}$ |

Übergangsfunktion und 3dB-Grenzfrequenz



mit $K = L \cdot \frac{R_1 + R_2}{R_1 \cdot R_2} = 5,1 \text{ ps}$

$$|H(\omega)| = \frac{R_2}{R_1 + R_2} \frac{\omega K}{\sqrt{1 + (\omega K)^2}}$$

$$\Rightarrow f_{3dB} = \frac{\omega_{3dB}}{2\pi} = \frac{1}{2\pi K}$$

$$= \frac{1}{2\pi * 5,1 \text{ ps}} = 31,2 \text{ GHz}$$

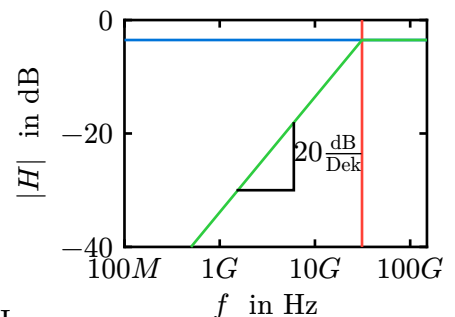
$$H(\omega \rightarrow \infty) = \frac{R_2}{R_1 + R_2} = \frac{2}{3} \quad | 20 \log(x)$$

$$= -3,51 \text{ dB}$$

$$H(\omega) = \frac{u_l}{u_e} = \frac{j\omega L \parallel R_2}{R_1 + (j\omega L \parallel R_2)}$$

$$= \frac{j\omega L \cdot R_2}{R_1 \cdot R_2 + j\omega L \cdot (R_1 + R_2)}$$

$$= \frac{R_2}{R_1 + R_2} \frac{j\omega K}{1 + j\omega K}$$



$H(\omega \rightarrow \infty) = -3,51 \text{ dB}$
 $f_{3dB} = 31,2 \text{ GHz}$

Feldeffekttransistor (FET)

$$r_{DS} = \frac{\partial U_{DS}}{\partial I_D} = \frac{|U_A| + U_{DS}}{I_D}$$

$$S = \frac{\partial I_D}{\partial U_{GS}} = \beta(U_{GS} - U_{th})$$

$$\beta = \mu \cdot C'_{ox} \cdot \frac{\omega}{l}$$

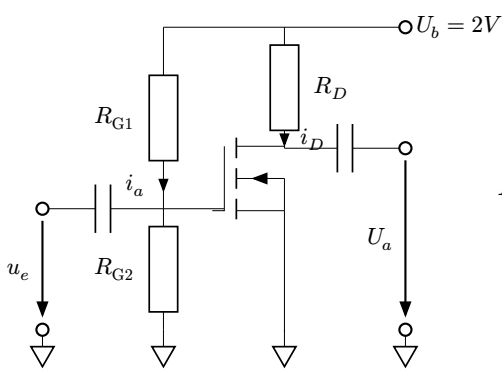
| | n-Kanal | p-Kanal |
|-----------------|---------|---------|
| normal leitend | | |
| normal sperrend | | |

Kleinsignalersatzschaltbild

$$I_D = \begin{cases} 0 & U_{GS} \leq U_{th} \\ \beta \cdot \left((U_{GS} - U_{th}) - \frac{U_{th}^2}{2} \right) \cdot \left(1 + \frac{U_{DS}}{U_A} \right) & \text{linearer Bereich} \\ \frac{\beta}{2} \cdot (U_{GS} - U_{th})^2 \cdot \left(1 + \frac{U_{DS}}{U_A} \right) & \text{Sättigungsbereich} \end{cases}$$

| Source-Schaltung | Gate-Schaltung | Drain-Schaltung |
|---|---|--|
| | | |
| $r_e = \infty$ $r_a = R_D \parallel r_{DS}$ $A = -S \cdot (R_D \parallel r_{DS})$ | $r_e = \frac{1}{S}$ $r_a = R_D \parallel r_{DS}$ $A = S \cdot (R_D \parallel r_{DS})$ | $r_e = \infty$ $r_a = \frac{1}{S} \parallel R_S$ $A = \frac{S \cdot R_S}{1 + S \cdot R_S}$ |

Arbeitspunkt und Lastgerade

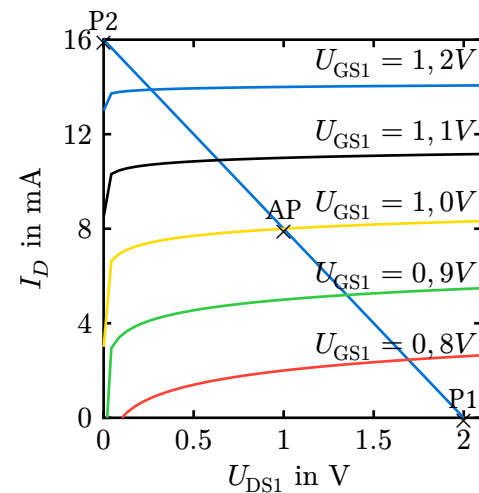


$$U_b = U_{DS1} + R_D \cdot I_D$$

$$\Leftrightarrow I_D = \frac{U_b - U_{DS1}}{R_D}$$

$$P1 : I_D(U_{DS1} = 0) = \frac{U_D}{R_D} = 16\text{mA}$$

$$P2 : I_D(U_{DS1} = U_b = 2\text{V}) = 0$$



Einstellen sodass $U_{GS1} = 1\text{V}$: $R_{G1} + R_{G2} = \frac{U_D}{I_D} \stackrel{!}{=} \frac{2\text{V}}{8\text{mA}} = 25\text{k}\Omega$

$$\frac{R_{G1}}{R_{G1} + R_{G2}} \stackrel{!}{=} U_{GS1} = 1\text{V}$$

$$\frac{R_{G2}}{R_{G1} + R_{G2}} \cdot U_D \stackrel{!}{=} U_D - U_{GS1} = 1\text{V} \Rightarrow R_{G1} = R_{G2} = 12,5\text{k}\Omega$$

NOT 1 AND & OR ≥ 1